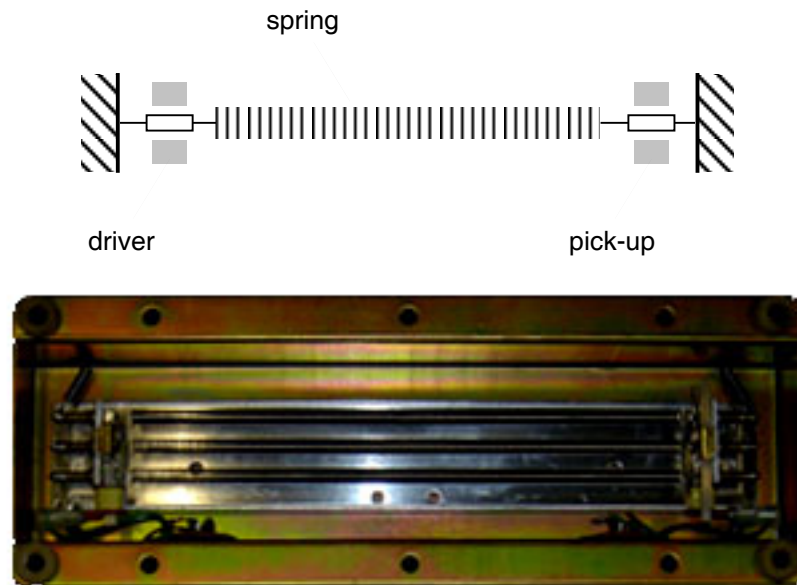


Robust Design of Very High-Order Allpass Dispersion Filters

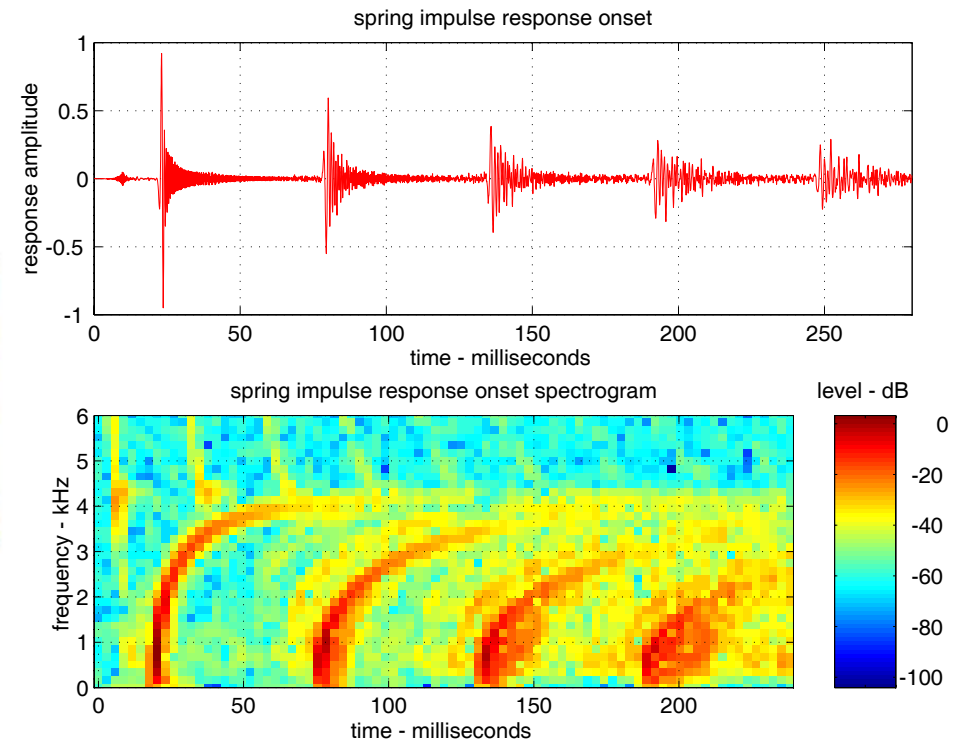
Jonathan S. Abel
abel@uaudio.com
Universal Audio, Inc.;
Stanford University

Julius O. Smith III
jos@ccrma.stanford.edu
CCRMA
Stanford University

Dispersive Propagation in a Spring Reverb

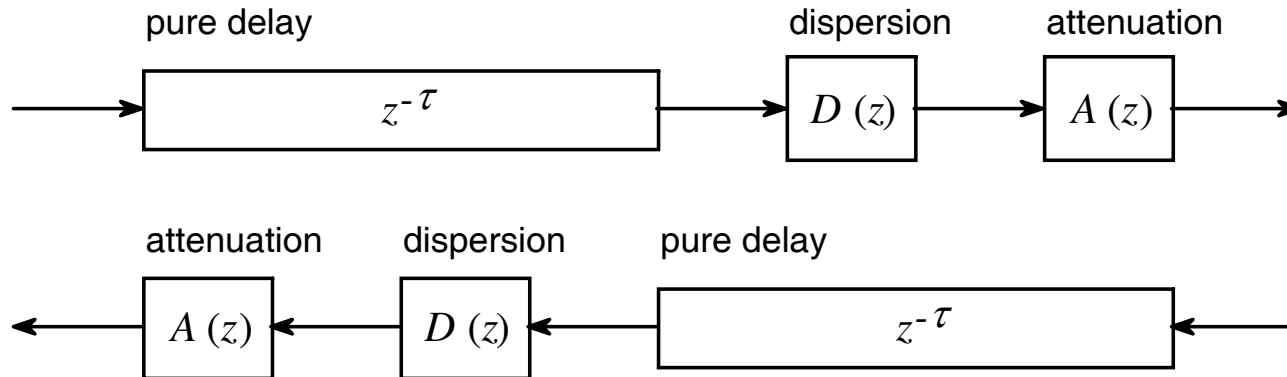
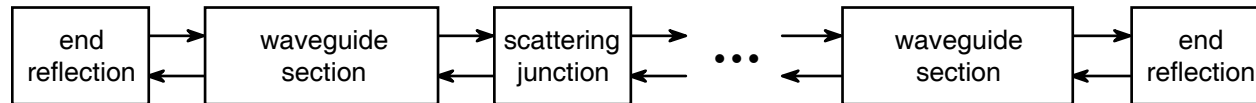
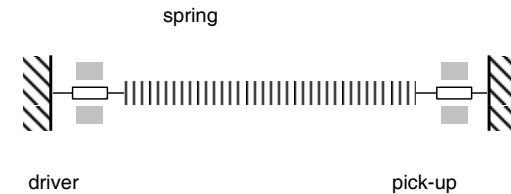


**Accutronics Type 8
Spring Reverberator**



- The torsional mode typically used by spring reverberators is highly dispersive, giving the spring its characteristic sound.

Dispersive Waveguide



- Each spring element is modeled using a set of dispersive waveguide sections.
- Left-going and right-going waves are separately processed via delay elements and commuted dispersion and loss filters.

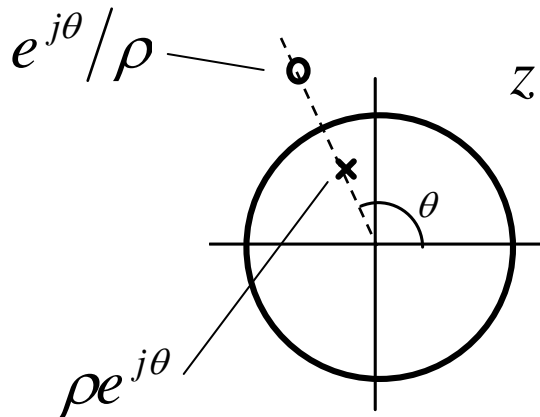
Allpass Dispersion Filter Design

$$G(z) = \frac{\rho_N + \rho_{N-1}z^{-1} + \dots + \rho_1z^{-N+1} + z^{-N}}{1 + \rho_1z^{-1} + \dots + \rho_{N-1}z^{-N+1} + \rho_Nz^{-N}}$$

- **Hilbert transform methods**
 - Yegnanarayana, IEEE-ASSP 1982
 - Reddy and Swamy, ICASSP 1998
 - Filter phase (not group delay) matched
 - Potential time aliasing, numerical issues; not in factored form
- **Optimal filter design formulation**
 - Lang and Laakso, IEEE-CAS1 1994; Lang, IEEE-SP 1998
 - Rocchesso and Scalcon, IEEE-CAS 1996
 - Bensa et al., ASA 2004
 - Rauhala and Valamaki, IEEE-SPL 2006
 - Maximum order limited by numerical difficulties; expensive design

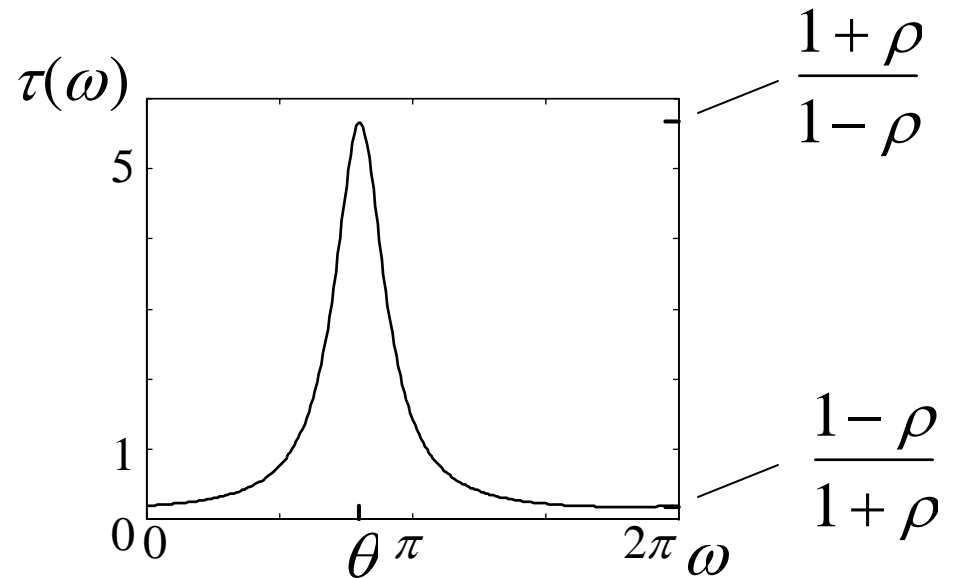


First-Order Allpass Filter



$$G(z) = \frac{-\rho e^{-j\theta} + z^{-1}}{1 - \rho e^{j\theta} \cdot z^{-1}}$$

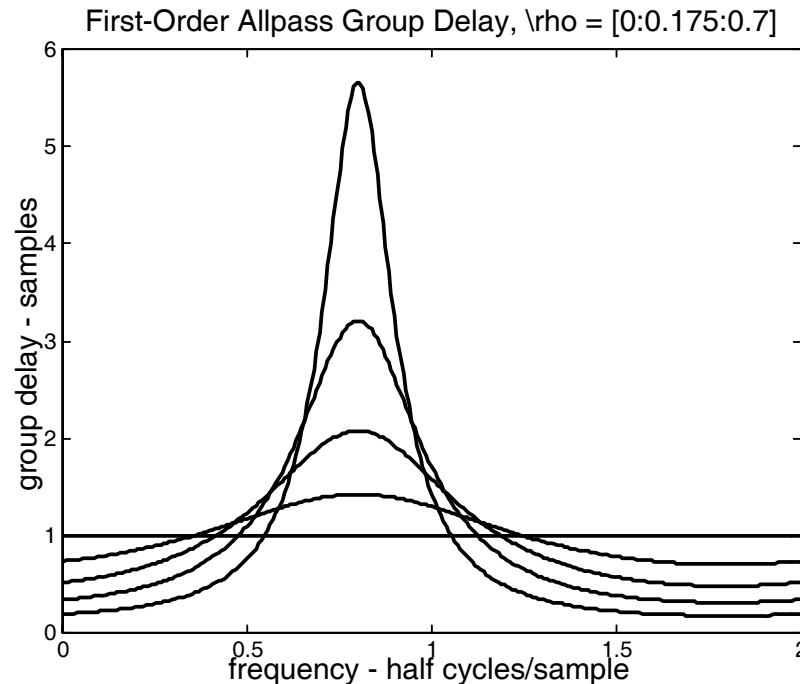
transfer function



$$\tau(\omega) = \frac{1 - \rho^2}{1 + \rho^2 - 2\rho \cos(\omega - \theta)}$$

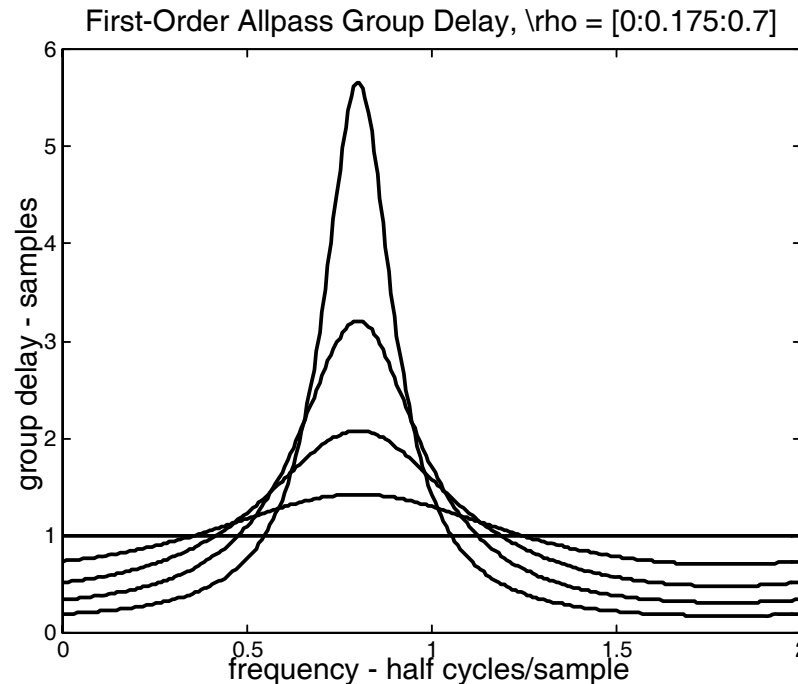
group delay

First-Order Allpass Group Delay



- As the pole is moved toward the unit circle, the first-order allpass group delay $\tau(\omega)$ becomes more peaked about the pole angle θ – the maximum increases, and the peak narrows.

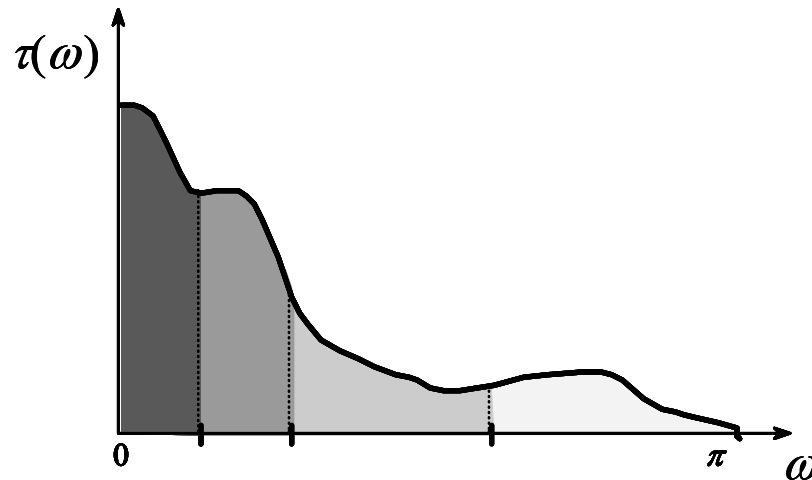
First-Order Allpass Group Delay



- The integral of the group delay $\tau(\omega)$ of a first-order allpass filter is 2π , independent of ρ and θ ,

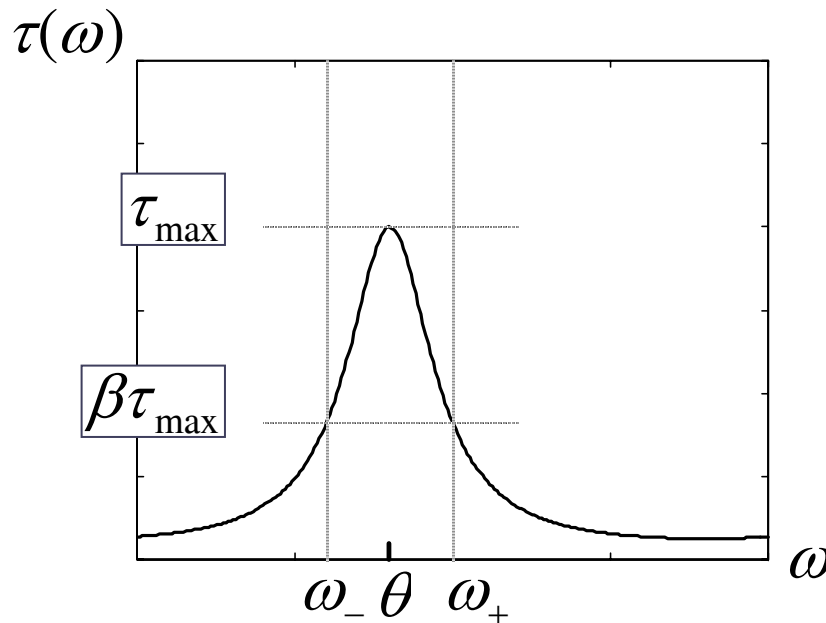
$$\int_0^{2\pi} \tau(\omega) d\omega = \varphi(2\pi) - \varphi(0) = 2\pi.$$

Allpass Filter Design Approach



- **Integrate $\tau(\omega)$, and add a constant delay τ_0 such that $\tau(\omega) + \tau_0$ integrates to a multiple of 2π .**
- **Divide $\tau(\omega) + \tau_0$ into 2π -area frequency bands.**
- **Fit a first-order allpass filter section to each band.**

First-Order Allpass Design



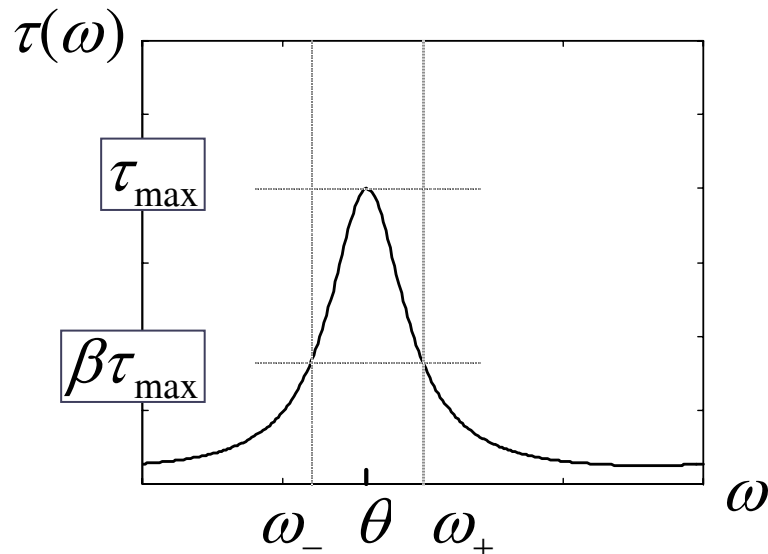
$$\rho = \eta - [\eta^2 - 1]^{1/2}$$

$$\eta = \frac{1 - \beta \cos \delta}{1 - \beta}$$

$$\delta = (\omega_- - \omega_+) / 2$$

- The pole angle θ is the band midpoint,
$$\theta = (\omega_- + \omega_+) / 2$$
- The section pole radius ρ is chosen to make the band edge group delay a fraction β of its maximum.

Dispersion Filter Design Cost

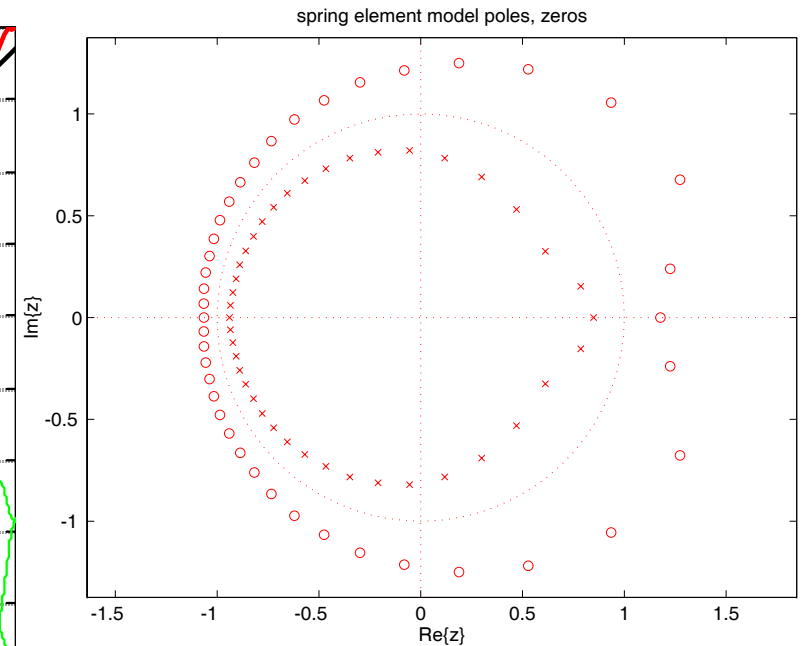
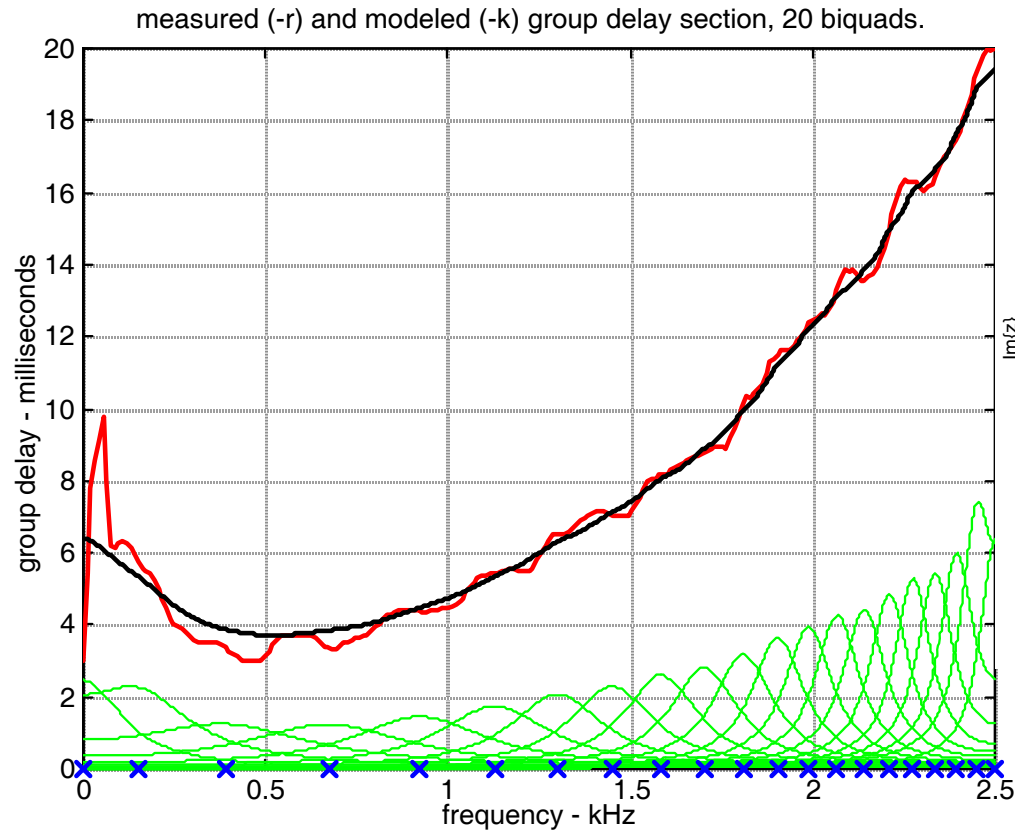


$$\rho \approx 1 - \left[\frac{\beta}{1 - \beta} \right]^{1/2} \delta, \quad \delta \ll 1$$

$$\delta = \frac{1}{2} |\omega_+ - \omega_-|$$

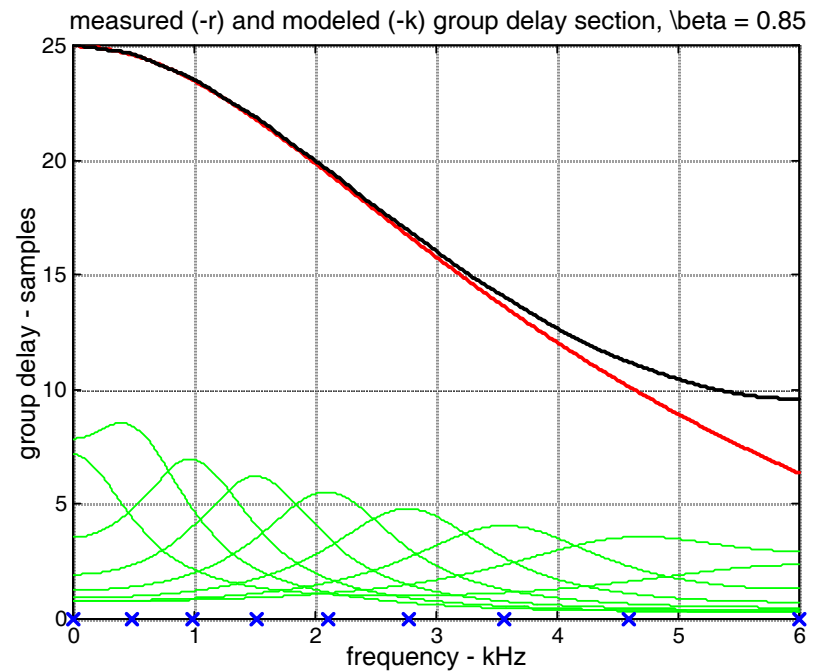
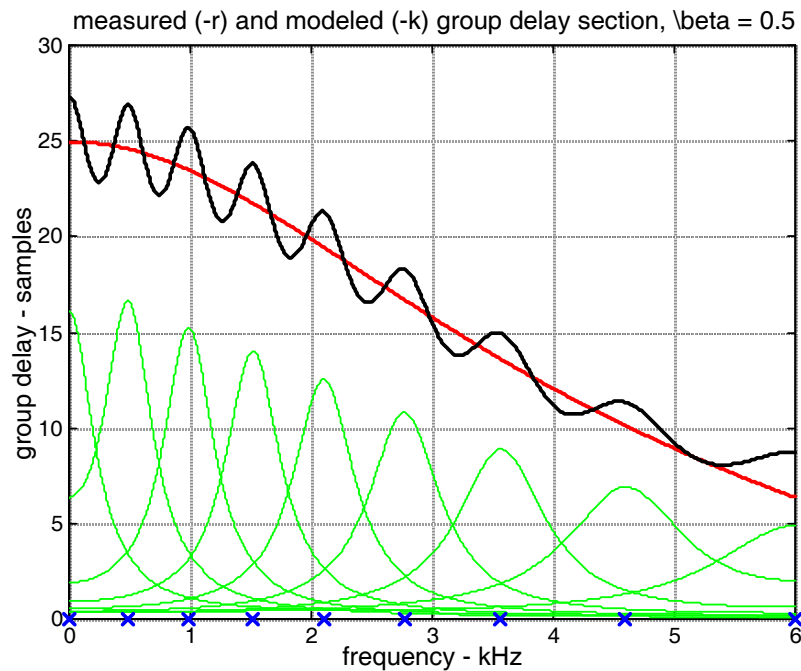
- **The design method is very inexpensive and may be used to update dispersion filters in real time.**
 - The pole angles θ_k directly encode the dispersive delay $\tau(\omega)$, and may be efficiently computed.
 - The pole radii $\rho_k(\beta)$ control delay smoothing, and are roughly linear in section bandwidth.

Design Example: Spring Reverberator Element



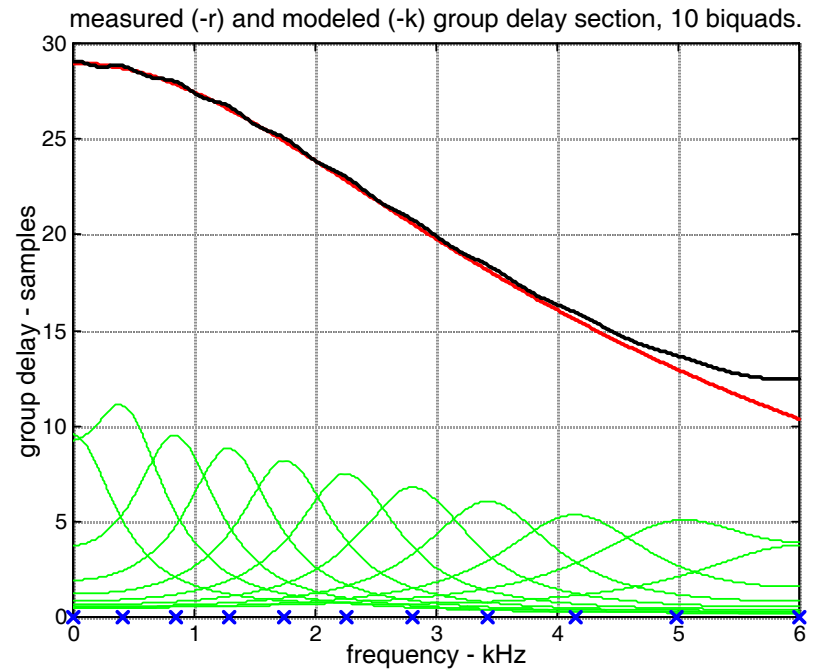
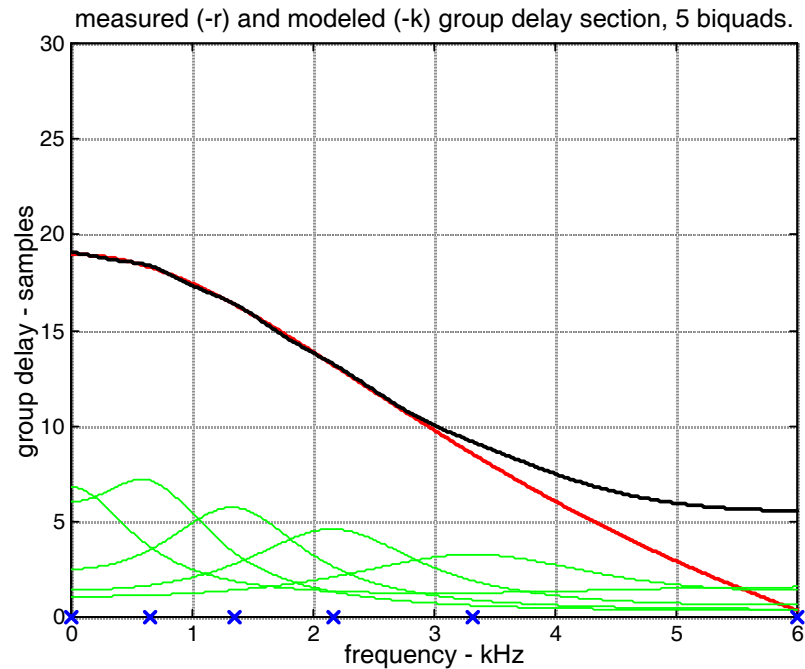
- **Poles, zeros follow smooth trajectories.**

Adjusting β



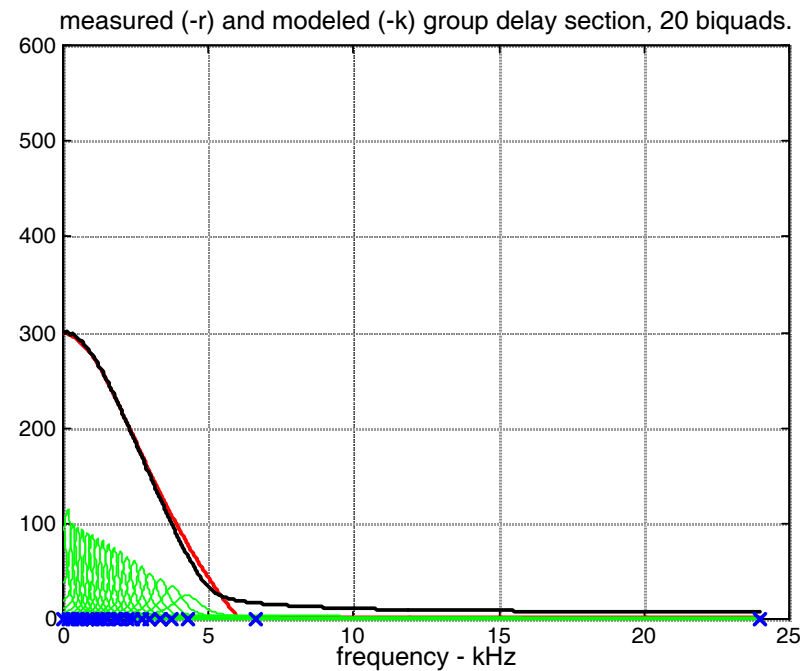
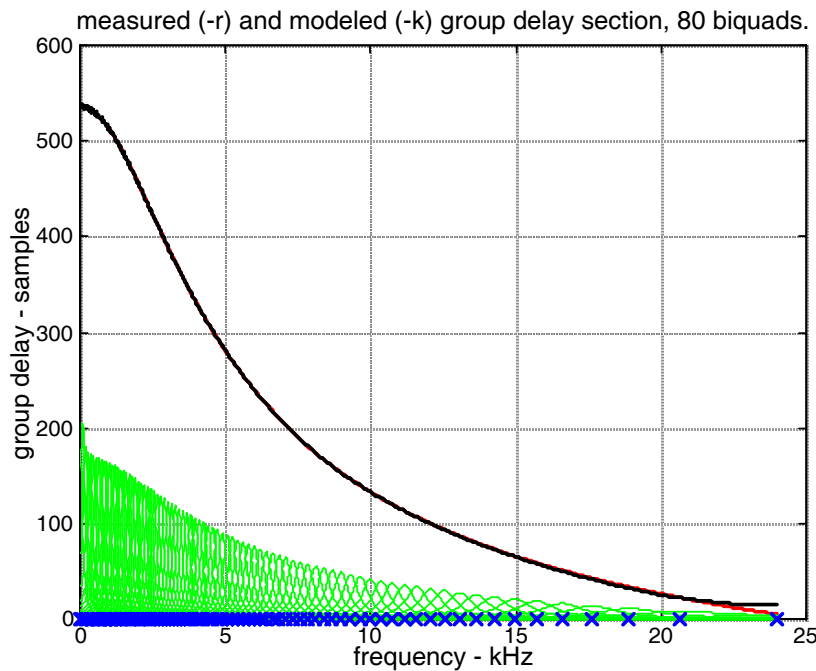
- Adjusting β trades ripple for responsiveness to narrow-band group delay changes.

Increasing Model Order



- Adding a constant delay τ_0 to the group delay $\tau(\omega)$ allows additional allpass sections to be used, and provides a more accurate fit.

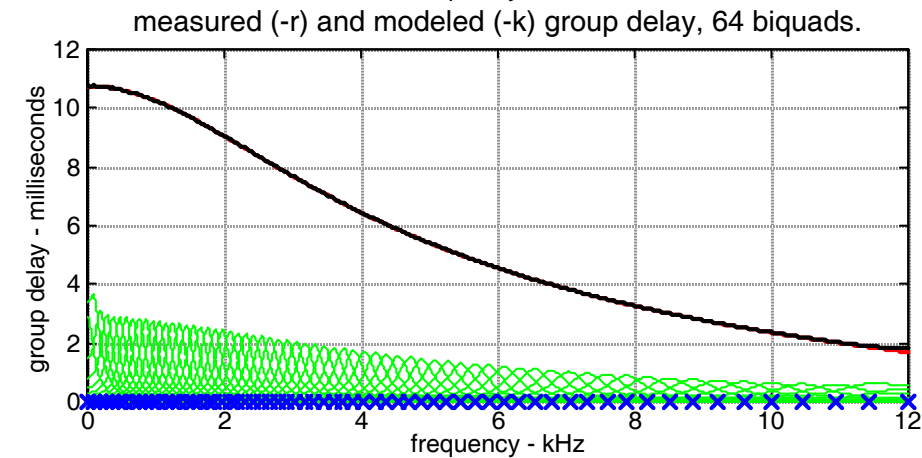
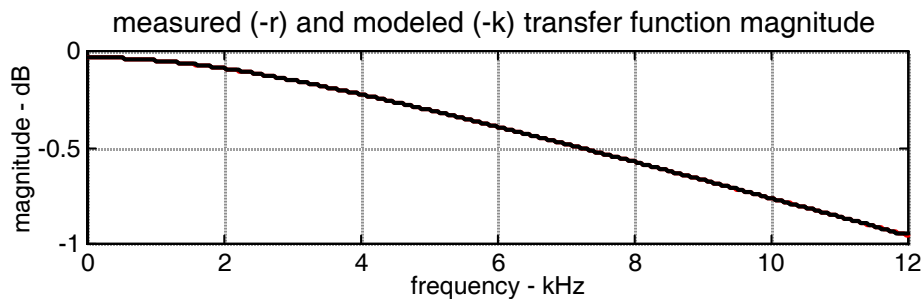
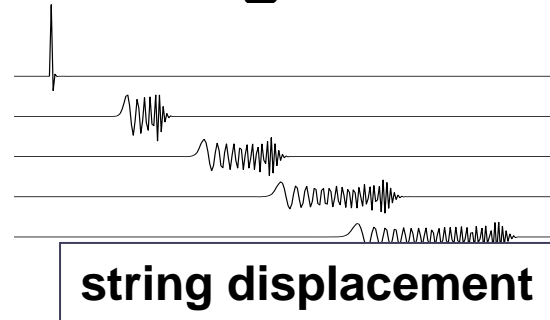
Low-Frequency Modeling



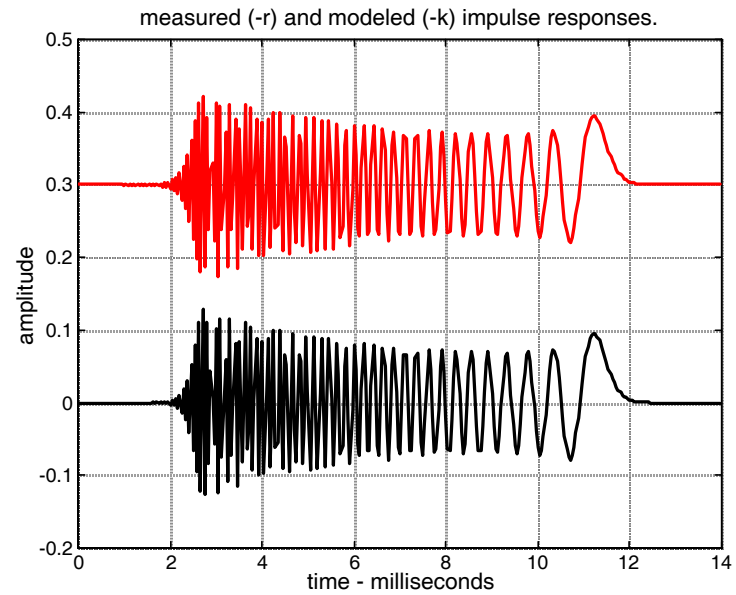
- **By setting $\tau(\omega) = 0$ outside the band of interest, the model order may be reduced.**

Piano String Propagation Filter Design

$$\exp\{-\alpha(\omega) \cdot d - j[\omega / c_0 - \varphi(\omega)] \cdot d\}$$



transfer functions



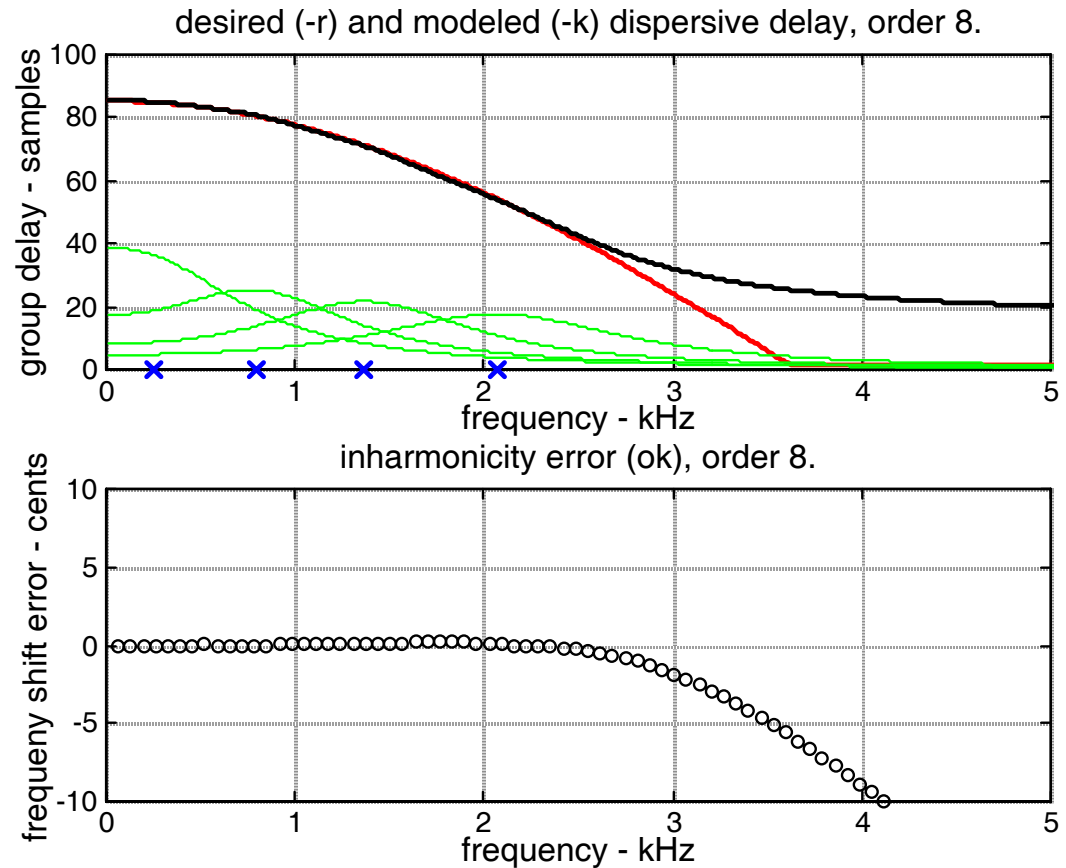
impulse responses



Stiff String Propagation Filter Design

$$\tau(\omega) = \frac{\tau_0}{\sqrt{1 + B\omega^2}}$$

$$\varphi(\omega) = \frac{\tau_0}{\sqrt{B}} \cdot \operatorname{asinh} \sqrt{B}\omega$$



Summary

- **New method for allpass dispersion-filter design:**
 - **Simple, numerically robust, nonparametric**
 - **Model order automatically determined**
 - **Filters produced in factored biquad form**
- **Future work**
 - **Applications**
 - Strings, springs and tubes of all kinds
 - Filter group-delay equalization
 - **Extensions**
 - Multiband group-delay filter design
 - Time-varying group-delay design
 - Frequency-dependent smoothing parameter β

